

Linearization

Most systems have non-linear behavior. When the behavior is represented by a smooth curve, and not sudden changes, linear approximations can be effectively employed in control theory.

We use Taylor's approximation as follows:

$$\text{Let } y = 4x^2 + 3x + 12$$

Exact values of y at $x=10$ and $x=11$ are

$$y_{10} = 4x^2 + 3x + 12 = 4.100 + 3.10 + 12 = 442$$

$$y_{11} = 4.11^2 + 3.11 + 12 = 484 + 33 + 12 = 529$$

Suppose we wish to use the system model where $x=10$

We will find y_{11} by linear approximation

$$Y = f(x_0) + \left(\frac{df}{dx}\right)(x - x_0) + \frac{d^2f}{dx^2} \left(\frac{(x-x_0)^2}{2!}\right)$$

$$\cong f(x_0) + \left(\frac{df}{dx}\right)(x - x_0)$$

Apply this for the given equation to find y_{11} when the neighbouring value y_{10} is known

$$y_{11} = y_{10} + \frac{dy}{dx} \cdot (x - x_0)$$

$$\frac{dy}{dx} = 8x + 3 = 8.10 + 3 = 83$$

$$y_{11} = y_{10} + 83 \cdot (11-10)$$

$$= 442 + 83 = 525$$

Which is close to the actual value of 529, and the linear approximation is acceptable.

Linearization for a function of two variables

Process is similar, except that Taylor's formula for the 2-variable case is used.

$$Y = f(x,y) = f(x_0, y_0) + \frac{df}{dx}(x - x_0) + \frac{df}{dy}(y - y_0)$$

$$\text{or } y = y_0 + K_1 \Delta x + K_2 \Delta y$$

leaving out 2nd order differential terms. Thus we can linearize a non-linear function of two variables about the point (x_0, y_0) .

Advantages of feedback

- 1) Output tracking: In open-loop, an input R is given from the knowledge of $G(s)$ and an output is obtained. If C is different, for any reason, due to error in $G(s)$ model or its variation due to changes in surroundings, C cannot be corrected.

In closed-loop control error is feedback to plant $G(s)$ if C is different from that expected, Error drives the plant $G(s)$ till C is the expected value for given R . Hence output is always improved, even if the parameters are varied.

- 2) System Response: System dynamics can be improved in a CL system.

For OL, $C(s)/R(s) = k/s+a$

Time constant, $T = 1/a$, & d.c. gain ($s=0$) is k/a

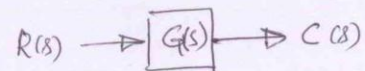
For CL case, $C(s)/R(s) = k_1/k_1+s+a$

For $R(s) = 1$, $C(s) = k_1/k_1+s+a$; $c(t) = k_1 e^{-(a+k_1)t}$

$T = 1/a+k_1$ & dc gain = $k_1/(k_1+a)$

Thus T , or speed of response can be controlled by varying K .

(Reduction of DC gain can be compensated by additional gain outside the loop)



- 3) Sensitivity to variation in parameters

Let the overall transfer function be $T(s)$

for OL, $T(s) = G(s)$; CL $\rightarrow T(s) = G/(1+GH)$

Sensitivity can be described as

$$S_G^T = \left(\frac{\partial T}{\partial G} \right) / \left(\frac{\partial T}{\partial G} \right) = \frac{\partial T}{\partial G} \cdot \frac{G}{T}$$

$$S_G^T = 1 \text{ for O.L system}$$

$$\text{For CL system, } S_G^T = \left(\frac{\partial T}{\partial G} \right) \cdot \frac{G}{T} = ((1+GH) - GH)/(1+GH)^2 \cdot (G/(G/(1+GH))) = 1/(1+GH)$$

Thus while it is 1 for OL system, it is $1/(1+GH)$ for CL system. CL system is less sensitive to variation in parameters.

CL system is also sensitive to variation in H . But the feedback elements are less costly and controlled more easily.

